

# Robust Tracking for a Class of Uncertain Switched Linear Systems Based on the Uncertainty and Disturbance Estimator

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**Abstract**—The robust tracking problem of a class of linear switched systems with both model uncertainty and external disturbance is investigated. Firstly, some new stability results for the linear switched systems with external disturbance are obtained in the following two cases: one is under arbitrary switching paths, the other is under switching paths with average dwell time. Secondly, a robust switched control strategy based on the existing uncertainty and disturbance estimator (UDE)-based control method is developed for a class of linear switched system with both model uncertainty and external disturbance. The asymptotic stability of the closed-loop linear switched system is established under the above two mentioned switching paths. Finally, the important features and good performance of the proposed method are demonstrated through numerical simulation studies.

## I. INTRODUCTION

In the past decades, switched systems and their applications have attracted considerable attention, and many important results have been published for the synthesis and analysis of those switched systems, e.g., [1], [2], [3], [4], [5], [6], [7], [8], [9], [10], [11], [12] and the references therein. Many efforts have been devoted to the linear switched systems described by linear difference or equations in the following aspects: stability [1], [2], [3], observability [4], controllability [5], stabilization [7], [6], [8], and so forth. There are two important methods to deal with the switched system: one is the common Lyapunov function (CLF) method [9], [10]; the other is the multiple Lyapunov functions (MLF) method [11]. According to the CLF method, for a given switched system if there exists a CLF, this switched system is globally asymptotically stable (GAS) under arbitrary switching laws if all subsystems are GAS. The MLF method is another powerful tool to investigate the stability problem of such switched systems in which all subsystems cannot share a CLF. For a given switched system whose subsystems cannot share a CLF, it is well known that such a system is GAS for any switching path if the dwell time, in which all the subsystems are active, is sufficiently large, and this method is called the dwell time (DT) method. Later, the average dwell time (ADT) method is proposed, and becomes a powerful tool to study the synthesis and analysis of those switched systems whose subsystems cannot share a CLF. Recently, an modified ADT method [12] is presented to

improve the existing ADT method in the following two aspects: 1) The application conditions of the existing ADT method is simplified; 2) The conservativeness in estimating the minimum lower bound of ADT is relaxed.

It should be noticed that among the above mentioned switched systems, system uncertainty and external disturbance are not considered. Unfortunately, this is not the case in practice. As a matter of fact, model uncertainty and external disturbance appear frequently in practical applications, and may deteriorate the performance (e.g., system stability, robustness of tracking). For the switched systems, a lot of methods have been proposed to investigate the robust stability and stabilization problems under both arbitrary switching and some specifically designed switching paths [13], [14], [15], [16], [17], [18], [19], [20], [21]. For example, model reference robust adaptive control (MRRAC) [13], adaptive robust control [14], sliding-mode control [15], [16], the disturbance-observer-based control (DOBC) [17], robust fault detection observer (RFDO) [18],  $H_\infty$  control [19], [20], [21], and so on. However, the assumption that the disturbance is bounded in some forms is required in most of above methods. For example,  $d(t)$  in [17] belongs to  $L_2^n[0, +\infty)$ , or  $d(t)$  in [18] is assumed to be  $L_2$ -norm bounded, etc. More importantly, the robust control and disturbance rejection problems in the above mentioned works are mainly solved by the linear matrix inequalities (LMIs). However, the stability conditions, which are derived by the LMIs, are only sufficient conditions and often result in the conservativeness of the conclusions. The robust control problem of linear switched systems with both model uncertainty and external disturbance has remained a very challenging problem.

The UDE-based control method [22] was proposed to replace the time-delay control (TDC) [23], and it has the following two advantages: 1) the system model or a disturbance model is not necessarily known completely; 2) both structured (or unstructured) uncertainties and external disturbances can be well handled. Being an effective robust control strategy, UDE-based control has found widespread applications in various non-switched systems, [24], [25], [26], [27]. Naturally, it is of interest to apply the UDE-based control to switched systems with both model uncertainty and external disturbance. To the best of the authors' knowledge, this problem has not been addressed in the existing literature. Therefore, the main goal of this paper is to develop a UDE-based switching control for the linear switched systems.

Motivated by the aforementioned discussions, the robust tracking problem will be studied thoroughly in this paper. Based on the CLF method, MLF method, and the obtained new stability results, the UDE-based switching control will be developed.

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Then, sufficient conditions to guarantee the asymptotic stability of the closed-loop linear switched system and the asymptotic tracking will be derived. The main contributions of this paper are summarized as follows: 1) some new stability results of the linear switched systems with disturbance are obtained in two cases: one is under arbitrary switching paths, the other is under switching paths with the restricted average dwell time; 2) the UDE-based control is used to study the robust tracking problem of the linear switched systems with both system uncertainty and external disturbance; 3) the UDE-based controllers are designed for each subsystem, and the whole closed-loop linear switched system is GAS for the aforementioned two cases.

## II. PRELIMINARIES AND PROBLEM FORMULATION

### A. Overview of the stability analysis of the linear switched time-invariant system

Consider the following linear switched time-invariant (LTI) system:

$$\dot{x}(t) = A_{\sigma(t)}x(t), \quad (1)$$

where  $x(t) \in R^n$  is the state vector,  $\sigma(t) : [0, \infty) \rightarrow \Lambda = \{1, 2, \dots, N\}$  is called the switching path, e.g.,  $\sigma(t) = i$  means that the  $i$ -th subsystem of the system (1) is active,  $A_i$  is the known matrix,  $i \in \Lambda$ ,  $\{t_m\}_{m=0}^{+\infty}$  is called the switching time sequence which is assumed to satisfy  $0 \leq t_0 < t_1 < \dots < t_n < \dots < +\infty$ . Let  $\tau_k = t_k - t_{k-1}$ , which is called the dwell time, where  $k \geq 1$ . In addition, it is assumed that the state of the linear switched system (1) is continuous, and only a finite number of switches can take place in any finite time interval.

Consider the linear switched system (1) in which all subsystems are stable. Some stability results are introduced.

*Lemma 1:* [1] Consider the linear switched system (1). If  $A_i$  shares a CLF  $V(x)$ , where  $i \in \Lambda$ , then the system (1) is GAS under arbitrary switching paths.

*Lemma 2:* [12] Consider the linear switched system (1). If  $V_i(x) = x^T P_i x$  is a Lyapunov function candidate of the  $i$ -th subsystem, where  $P_i > 0$ ,  $i \in \Lambda$ , then the system (1) is GAS under any switching path with the following restricted ADT:

$$\tau_a \geq \tau_a^* = \frac{a}{\lambda_0}, \quad (2)$$

where

$$a = \ln \mu, \mu = \max_{i \in \Lambda} \frac{\lambda_{\max}(P_i)}{\lambda_{\min}(P_i)}, \lambda_0 = \min_{i \in \Lambda} \lambda_i, \quad (3)$$

with  $\lambda_i > 0$  given as

$$\lambda_i = \frac{\lambda_{\min}(Q_i)}{\lambda_{\max}(P_i)},$$

and  $Q_i > 0$ ,  $i \in \Lambda$ , which satisfies the following condition:

$$P_i^T A_i + P_i A_i = -Q_i, i \in \Lambda. \quad (4)$$

### B. Problem Formulation

Consider the following switched system in which both model uncertainty and external disturbance exist:

$$\dot{x}(t) = (A_{\sigma(t)} + F_{\sigma(t)})x(t) + B_{\sigma(t)}u_{\sigma(t)}(t) + d_{\sigma(t)}(t), \quad (5)$$

where  $x(t) \in R^n$  is the state vector,  $A_i$  is the known state matrix,  $F_i$  is a matrix which is not known in advance and is called the model uncertainty,  $B_i$  is the control matrix which is assumed to have full column rank,  $(A_i, B_i)$  is a controllable pair,  $u_i(t) = (u_{i1}(t), u_{i2}(t), \dots, u_{ir}(t))^T \in R^r$  is the control input vector, and  $d_i(t)$  is the unpredictable external disturbance vector, of the  $i$ -th subsystem, respectively,  $i \in \Lambda$ .

The objective of this paper is to investigate the robust tracking problem of the switched system (5) by the UDE-based control method in the following two cases: one is under arbitrary switching paths, the other is under switching paths with the restricted average dwell time. In this paper, the tracked signal  $c(t) \in R^r$  is a given command, which is assumed to be a piecewise smooth (continuous) and uniformly bounded, for example, trigonometric functions.

## III. MAIN RESULTS

### A. Some new stability results of the linear switched systems with disturbance

Consider the following switched system with disturbance:

$$\dot{x}(t) = A_{\sigma(t)}x(t) + \tilde{u}_{d\sigma(t)}(t), \quad (6)$$

where  $x(t) \in R^n$  is the state vector,  $A_i$  is the known matrix, and  $\tilde{u}_{di}(t)$  is the external disturbance,  $i \in \Lambda$ .

Based on Lemma 1 and Lemma 2, some new results of the linear switched system (6) are obtained in the following.

*Theorem 1:* For the linear switched system (6), if the following conditions:

C1:  $A_i$ ,  $i \in \Lambda$ , are Hurwitz matrices, which implies that there exist  $L_1 > 0, L_2 > 0$  and  $\lambda > 0$  satisfying the condition:  $L_1 e^{-\lambda t} \leq \|e^{A_i t}\| \leq L_2 e^{-\lambda t}$ ,  $i \in \Lambda$ ;

C2:  $A_i A_j = A_j A_i$ ,  $i, j \in \Lambda$ ;

C3:  $\|\tilde{u}_{di}(t)\| \leq \alpha(t)$ ,  $i \in \Lambda$ , where  $\alpha(t)$  satisfies  $\int_0^{+\infty} e^{\lambda t} \alpha(t) dt < \infty$ ;

are satisfied, then the system (6) is GAS under arbitrary switching paths.

*Proof:* Let  $\sigma(t) = i_k$  for  $t \in [t_{k-1}, t_k)$ ,  $k \geq 1$ . From (6), it results in

$$\dot{x}(t) = A_{i_k}x(t) + \tilde{u}_{di_k}(t), t \in [t_{k-1}, t_k),$$

which implies that

$$x(t) = e^{A_{i_k}(t-t_{k-1})}x(t_{k-1}) + \int_{t_{k-1}}^t e^{A_{i_k}(t-s)}\tilde{u}_{di_k}(s)ds.$$

By induction, for  $t \in [t_{k-1}, t_k)$ , it results in

$$\begin{aligned} x(t) &= e^{A_{i_k}(t-t_{k-1})}e^{A_{i_{k-1}}(t_{k-1}-t_{k-2})}\dots e^{A_{i_1}(t_1-t_0)}x(t_0) \\ &+ \int_{t_0}^{t_1} e^{A_{i_k}(t-t_{k-1})}e^{A_{i_{k-1}}(t_{k-1}-t_{k-2})} \\ &\dots e^{A_{i_1}(t_1-s)}\tilde{u}_{di_1}(s)ds \\ &+ \int_{t_1}^{t_2} e^{A_{i_k}(t-t_{k-1})}e^{A_{i_{k-1}}(t_{k-1}-t_{k-2})} \\ &\dots e^{A_{i_2}(t_2-s)}\tilde{u}_{di_2}(s)ds \\ &+ \dots \int_{t_{k-1}}^t e^{A_{i_k}(t-s)}\tilde{u}_{di_k}(s)ds. \end{aligned}$$

Let  $\tau_i(0, t)$  be the total time of the  $i$ -th subsystem of the linear switched system (6) active during the time interval  $[0, t)$ . From condition C2, it follows that

$$\begin{aligned}
x(t) &= e^{A_1\tau_1(0,t)}e^{A_2\tau_2(0,t)}\dots e^{A_n\tau_n(0,t)}x(t_0) \\
&+ \int_{t_0}^{t_1} e^{A_1\tau_1(s,t)}e^{A_2\tau_2(s,t)}\dots e^{A_n\tau_n(s,t)}\tilde{u}_{di_1}(s)ds \\
&+ \int_{t_1}^{t_2} e^{A_1\tau_1(s,t)}e^{A_2\tau_2(s,t)}\dots e^{A_n\tau_n(s,t)}\tilde{u}_{di_2}(s)ds \\
&+ \dots \int_{t_{k-1}}^t e^{A_1\tau_1(s,t)}e^{A_2\tau_2(s,t)}\dots e^{A_n\tau_n(s,t)}\tilde{u}_{di_k}(s)ds.
\end{aligned}$$

Using conditions C1 and C3, it results in

$$\begin{aligned}
\|x(t)\| &\leq L_2^N e^{-\lambda t}\|x(t_0)\| + L_2^N \int_{t_0}^{t_1} e^{-\lambda(t-s)} \|\tilde{u}_{di_1}(s)\| ds \\
&+ L_2^N \int_{t_1}^{t_2} e^{-\lambda(t-s)} \|\tilde{u}_{di_2}(s)\| ds \\
&+ L_2^N \int_{t_2}^{t_3} e^{-\lambda(t-s)} \|\tilde{u}_{di_3}(s)\| ds \\
&+ \dots L_2^N \int_{t_{k-1}}^t e^{-\lambda(t-s)} \|\tilde{u}_{di_k}(s)\| ds \\
&\leq L_2^N \left( e^{-\lambda t}\|x(t_0)\| + \int_{t_0}^t e^{-\lambda(t-s)} \alpha(s) ds \right) \\
&= e^{-\lambda t} L_2^N \left( \|x(t_0)\| + \int_{t_0}^t e^{\lambda s} \alpha(s) ds \right).
\end{aligned}$$

Thus,  $\lim_{t \rightarrow \infty} \|x(t)\| = 0$ . This completes the proof.  $\blacksquare$

*Remark 1:* The condition:  $\int_0^{+\infty} e^{\lambda t} \alpha(t) dt < \infty$ , implies that  $\alpha(t) = o(e^{-\lambda t})$ . Moreover, according to the equation (6), there exists a constant  $L_3 > 0$  such that  $L_3 \|e^{A_i t}\| \leq \|x(t)\|$ ,  $i \in \Lambda$ . Thus, an appropriate  $\alpha(t)$  and a positive constant  $\varepsilon$  are chosen to satisfy the condition:  $\alpha(t) \leq \varepsilon \|x\|$ . For example,

$$\alpha(t) = \varepsilon L_3 L_1 e^{-(\lambda+1)t} \leq \varepsilon L_3 L_1 e^{-\lambda t} \leq \varepsilon L_3 \|e^{A_i t}\| \leq \varepsilon \|x(t)\|.$$

Next, the condition C2 is relaxed to the following condition:

C4: There exist a group of matrices  $Q_i > 0$ ,  $P > 0$ , such that

$$P^T A_i + A_i P = -Q_i, i \in \Lambda, \quad (7)$$

which implies that  $V(x) = x^T P x$  is a CLF for the linear switched system:  $\dot{x}(t) = A_{\sigma(t)} x(t)$ .

In this case, one possible choice for  $\alpha(t)$  is

$$\alpha(t) = \varepsilon_1 L_3 L_1 e^{-(\lambda+\varepsilon)t}, \quad (8)$$

which implies that  $\alpha(t) \leq \varepsilon_1 \|x(t)\|$ , where  $\varepsilon$  is an arbitrary positive number, and  $\varepsilon_1$  is determined by

$$\varepsilon_1 = \frac{\lambda_{\min}}{2\lambda_{\max}(P)}, \lambda_{\min} = \min_{i \in \Lambda} \{\lambda_{\min}(Q_i)\}. \quad (9)$$

For the linear switched system (6), a conclusion is obtained as follows.

*Theorem 2:* Consider the linear switched system (6). If the conditions C1, C3 and C4 are satisfied, where  $\alpha(t)$  is given in (8), then the system (6) is GAS under arbitrary switching paths.

*Proof:* Let  $V(x) = x^T P x$ , using the conditions C1, C4 and  $\alpha(t)$ , then it results in

$$\begin{aligned}
\dot{V}(x(t)) &= \dot{x}^T(t) P x(t) + x^T(t) P \dot{x}(t) \\
&= x^T(t) (A_i^T P + P A_i) x(t) + \tilde{u}_{di}^T(t) P x(t) \\
&\quad + x^T(t) P \tilde{u}_{di}(t) \\
&= -x^T(t) Q_i x(t) + 2x^T(t) P \tilde{u}_{di}(t) \\
&\leq -\lambda_{\min} \|x(t)\|^2 + 2\lambda_{\max}(P) \|x(t)\| \|\tilde{u}_{di}(t)\| \\
&\leq -\lambda_{\min} \|x(t)\|^2 + 2\lambda_{\max}(P) \|x(t)\| \alpha(t) \\
&\leq -\lambda_{\min} \|x(t)\|^2 + 2\varepsilon_1 \lambda_{\max}(P) \|x(t)\|^2 \\
&= -(\lambda_{\min} - \lambda_{\min}) \|x(t)\|^2 \\
&= 0.
\end{aligned} \quad (10)$$

Thus, the system (6) is GAS under arbitrary switching paths.  $\blacksquare$

As for the linear switched system (6), if only the conditions C1 and C3 are satisfied, one possible choice for  $\alpha(t)$  is

$$\alpha(t) = \varepsilon_2 L_3 L_1 e^{-(\lambda+\varepsilon)t}, \quad (11)$$

which implies that  $\alpha(t) \leq \varepsilon_2 \|x(t)\|$ , where  $\varepsilon$  is an arbitrary positive number, and  $\varepsilon_2$  is determined by

$$\varepsilon_2 = \max_{i \in \Lambda} \left\{ \frac{\lambda_{\min}(Q_i) - l_i \lambda_{\max}(P_i)}{2\lambda_{\max}(P)} \right\}, \quad (12)$$

with  $l_i > 0$ , which is chosen in advance to meet the following condition:

$$\lambda_{\min}(Q_i) - l_i \lambda_{\max}(P_i) > 0, i \in \Lambda, \quad (13)$$

and  $P_i > 0$ ,  $Q_i > 0$ , are given in (4),  $i \in \Lambda$ .

*Theorem 3:* Consider the linear switched system (6). If the conditions C1 and C3 are satisfied, where  $\alpha(t)$  is given in (11), then the linear switched system (6) is GAS under any switching path with ADT  $\tau_a \geq \tau_a^*$ , where  $\tau_a^*$  is designed as

$$\tau_a^* = \frac{a}{l_0}, \quad (14)$$

with

$$a = \ln \mu, \mu = \max_{i \in \Lambda} \left\{ \frac{\lambda_{\max}(P_i)}{\lambda_{\min}(P_i)} \right\}, l_0 = \min_{i \in \Lambda} \{l_i\}, \quad (15)$$

and  $P_i, Q_i$  given in (4),  $l_i$  is given in (12),  $i \in \Lambda$ .

*Proof:* Let  $V_i(x) = x^T P_i x$ , using the condition C1, the equation (4) and  $\alpha(t)$ , it follows

$$\begin{aligned}
\dot{V}_i(x(t)) &= \dot{x}^T(t) P_i x(t) + x^T(t) P_i \dot{x}(t) \\
&= x^T(t) (A_i^T P_i + P_i A_i) x(t) + \tilde{u}_{di}^T(t) P_i x(t) \\
&\quad + x^T(t) P_i \tilde{u}_{di}(t) \\
&= -x^T(t) Q_i x(t) + 2x^T(t) P \tilde{u}_{di}(t) \\
&\leq -\lambda_{\min}(Q_i) \|x(t)\|^2 + 2\lambda_{\max}(P_i) \|x(t)\| \|\tilde{u}_{di}(t)\| \\
&\leq -\lambda_{\min}(Q_i) \|x(t)\|^2 + 2\lambda_{\max}(P_i) \|x(t)\| \alpha(t) \\
&\leq -\lambda_{\min}(Q_i) \|x(t)\|^2 + 2\varepsilon_2 \lambda_{\max}(P_i) \|x(t)\|^2 \\
&= -\lambda_{\min}(Q_i) \|x(t)\|^2 \\
&\quad + 2\lambda_{\max}(P_i) \frac{\lambda_{\min}(Q_i) - l_i \lambda_{\max}(P_i)}{2\lambda_{\max}(P)} \|x(t)\|^2 \\
&\leq -l_i \lambda_{\max}(P_i) \|x(t)\|^2 \\
&\leq -l_i V_i(x(t)).
\end{aligned} \quad (16)$$

According to the proof of Lemma 2, the system (6) is GAS under any switching path with ADT  $\tau_a \geq \tau_a^*$ . This completes the proof.  $\blacksquare$

*B. Robust tracking problem of linear switched system with both model uncertainty and external disturbance by the UDE-based control method*

In this subsection, the robust tracking problem of the switched system (5) is investigated by the UDE-based control method in refs [24], [25], [26], [27]. The control design involves two steps. The first step is to design a switched reference model which is given as

$$\begin{aligned}
\dot{x}_m(t) &= (A_{\sigma(t)} + B_{\sigma(t)} K_{\sigma(t)}) x_m(t) + B_{m\sigma(t)} c_{\sigma(t)}(t) \\
&\quad + D_{m\sigma(t)} \dot{c}(t),
\end{aligned} \quad (17)$$

where  $x_m(t) \in R^n$  is the reference state vector,  $\sigma(t)$  is the switching path,  $c(t) = (c_1(t), c_2(t), \dots, c_r(t))^T \in R^r$  is a given command, which is piecewise smooth and uniformly bounded to the  $i$ -th subsystem,  $K_i$  is the feedback gain matrix of the  $i$ -th subsystem with appropriate dimension, which is chosen in advance to make the matrix  $A_i + B_i K_i$  be Hurwitz, and  $B_{mi} = -M_{i1}$ , where  $M_{i1}, M_{i2}$  are the blocks of matrix  $A_i + B_i K_i$ , i.e.,

$$A_i + B_i K_i = (M_{i1}, M_{i2}), D_{mi} = \begin{pmatrix} I_r \\ 0 \end{pmatrix} \in R^{n \times r}, i \in \Lambda.$$

Then, the desired switched error system is described as follows:

$$\dot{e}(t) = (A_{\sigma(t)} + B_{\sigma(t)} K_{\sigma(t)})e(t). \quad (18)$$

The second step is to design controllers  $u_i, i \in \Lambda$ . According to the results in refs [24], [25], [26], [27], the UDE-based control law for the  $i$ -th subsystem of the linear switched system (5) can be obtained as

$$\begin{aligned} u_i(t) = & B_i^+ \mathcal{L}^{-1} \left[ \frac{1}{1-G_{fi}(s)} \right] * B_i K_i x(t) \\ & + B_i^+ \mathcal{L}^{-1} \left[ \frac{1}{1-G_{fi}(s)} \right] * [B_{mi} c(t) + D_{mi} \dot{c}(t)] \\ & - B_i^+ \left\{ \mathcal{L}^{-1} \left[ \frac{s G_{fi}(s)}{1-G_{fi}(s)} \right] * x(t) \right\} \\ & + B_i^+ \left\{ \mathcal{L}^{-1} \left[ \frac{G_{fi}(s)}{1-G_{fi}(s)} \right] * (A_i x(t)) \right\}, \end{aligned} \quad (19)$$

where  $B_i^+ = (B_i^T B_i)^{-1} B_i^T$  is the pseudo-inverse of  $B_i$ ,  $\mathcal{L}^{-1}\{\cdot\}$  is the inverse Laplace transform operator, and  $G_{fi}(s)$  is a strictly proper stable filter with the appropriate frequency characteristics for the  $i$ -th subsystem of the linear switched system (5),  $i \in \Lambda$ .

According to Theorem 1, the following conclusion is obtained.

**Theorem 4:** Consider the system (5) and reference model (17). If  $B_i K_i = S_i - A_i$ , where  $S_i, i \in \Lambda$ , are Hurwitz and pairwise commutative, i.e.,  $S_i S_j = S_j S_i, i, j \in \Lambda$ , and the filter  $G_{fi}(s)$  is designed to make  $\tilde{u}_{di}$  satisfy the condition C3,  $i \in \Lambda$ , then the state  $x(t)$  of the switched system (5) asymptotically tracks the state  $x_m(t)$  of the switched reference model (17) under arbitrary switching paths.

*Proof:* If  $B_i K_i = S_i - A_i$ , i.e.,  $A_i + B_i K_i = S_i, i \in \Lambda$ , then the switched reference model is given as

$$\dot{x}_m(t) = S_{\sigma(t)} x_m(t) + B_{m\sigma(t)} c(t) + D_{m\sigma(t)} \dot{c}(t). \quad (20)$$

Substituting the controller  $u(t)$  given in (19) into the system (5), then the switched error dynamics becomes

$$\dot{e}(t) = S_i e(t) - \tilde{u}_{di}(t), \quad (21)$$

where  $\tilde{u}_{di}$  is the estimated error (the difference between the uncertainty and disturbance term and their estimated value) of the  $i$ -th subsystem, respectively,  $i \in \Lambda$ . Note that  $\tilde{u}_{di}$  satisfies the condition C3,  $i \in \Lambda$ , thus the switched error dynamics in (21) is GAS under arbitrary switching paths according to Theorem 1. This completes the proof. ■

Based on Theorem 2, a conclusion is obtained as follows.

**Theorem 5:** Consider the system (5) and the reference model (17). If  $B_i K_i = S_i - A_i$ , where  $S_i$  is Hurwitz,  $i \in \Lambda$ , and the

conditions: C3 and C4 are satisfied, where  $\alpha(t)$  is given in (8), then the state  $x(t)$  of the switched system (5) asymptotically tracks the state  $x_m(t)$  of the switched reference model (17) under arbitrary switching paths.

*Proof:* Similarly, the obtained switched error dynamics is

$$\dot{e}(t) = S_i e(t) - \tilde{u}_{di}(t), \quad (22)$$

where  $\tilde{u}_{di}$  is the estimated error the  $i$ -th subsystem, respectively,  $i \in \Lambda$ . Note that  $R_i$  is Hurwitz,  $i \in \Lambda$ , and the conditions: C3 and C4 are satisfied, where  $\alpha(t)$  is given in (8), thus the switched error dynamics in (22) is GAS under arbitrary switching paths according to Theorem 2, which completes the proof. ■

For the system (5), if  $A_i + B_i K_i = S_i$ , where  $S_i$  is Hurwitz,  $i \in \Lambda$ , but the condition: C4 is not satisfied, the following result is obtained according to Theorem 3.

**Theorem 6:** Consider the system (5) and the reference model (17). If  $B_i K_i = S_i - A_i$ , where  $S_i$  is Hurwitz,  $i \in \Lambda$ , and the condition: C3 is satisfied, where  $\alpha(t)$  is given in (11), then the state  $x(t)$  of the switched system (5) asymptotically tracks the state  $x_m(t)$  of the switched reference model (17) under any switching signal with ADT  $\tau_a$ , where  $\tau_a^*$  is determined by the equations (3) and (4).

*Proof:* Similarly, the obtained switched error dynamics is

$$\dot{e}(t) = S_i e(t) - \tilde{u}_{di}(t), \quad (23)$$

where  $\tilde{u}_{di}$  is the estimated error of the  $i$ -th subsystem, respectively,  $i \in \Lambda$ . Note that the matrices  $S_i, i \in \Lambda$ , are Hurwitz, and the condition: C3 is satisfied, where  $\alpha(t)$  is given in (11), thus the switched system in (23) is GAS under any signal with the restricted ADT  $\tau_a$  according to Theorem 2. ■

It should be noticed that the filters  $G_{fi}(s), i \in \Lambda$ , which guarantee  $\tilde{u}_{di}$  satisfy the condition C3, especially for  $\alpha(t)$  given in (8) and (11), are designed according to the results in [27]. The good performance will be shown by the simulation studies in Section IV.

#### IV. SIMULATION STUDIES

In this section, the numerical validation is carried out for an example in which the matrices of the closed loop linear switched systems cannot share a CLF.

Consider the following linear switched system with both model uncertainty and external disturbance:

$$\dot{x} = (A_{\sigma(t)} + F_{\sigma(t)})x + B_{\sigma(t)}u_{\sigma(t)}(t) + d_{\sigma(t)}(t), \quad (24)$$

where  $\Lambda = \{1, 2\}$ ,

$$A_1 = \begin{pmatrix} 0 & 1 \\ 12 & -11 \end{pmatrix}, A_2 = \begin{pmatrix} -2 & 13 \\ 10 & 1 \end{pmatrix}, \\ B_1 = B_2 = \begin{pmatrix} 1 \\ 1 \end{pmatrix},$$

$$F_1 = \begin{pmatrix} 0.02 & 0 \\ 0 & 0.12 \end{pmatrix}, F_2 = \begin{pmatrix} 0.1 & 0 \\ 0 & 0.11 \end{pmatrix},$$

and

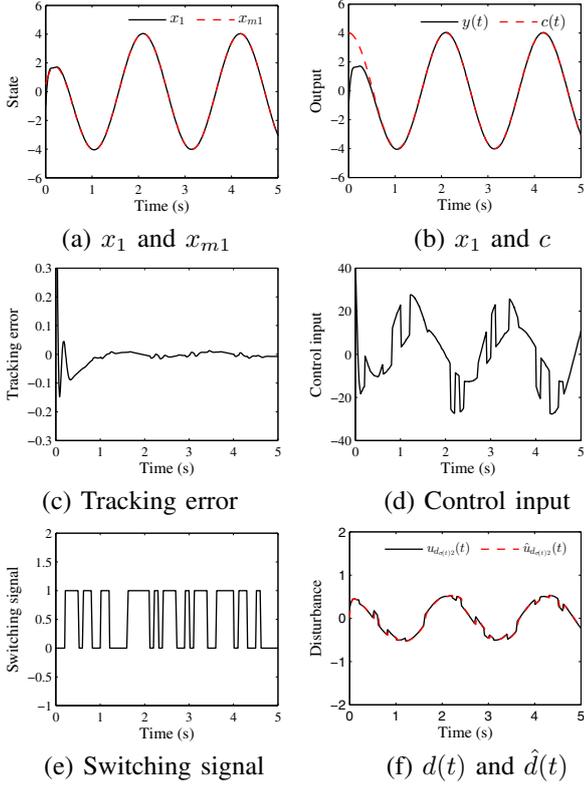


Figure 1. The results of the UDE-based robust tracking performance of switched system (24) where the matrices of the closed loop switched systems cannot share CLF.

$$d_1(t) = \begin{pmatrix} 0.1 \sin(0.1t) \\ 0.02 \cos(0.5t) \end{pmatrix}, d_2(t) = \begin{pmatrix} 0.02 \cos(0.1t) \\ 0.1 \sin(t) \end{pmatrix}.$$

The objective is to design the controller  $u_i(t)$  such that  $x_1(t)$  asymptotically tracks  $c(t) = \cos(5t)$ .

The first step is to design a linear switched reference system which is described as follows:

$$\dot{x}_m = (A_{\sigma(t)} + K_{\sigma(t)})x_m + B_{m\sigma(t)}c(t) + D_{m\sigma(t)}\dot{c}(t). \quad (25)$$

For the feedback gains  $K_i$ ,  $i \in \Lambda$ , one feasible choice is

$$K_1 = \begin{pmatrix} -11 & -11 \end{pmatrix}, K_2 = \begin{pmatrix} -20 & -12 \end{pmatrix},$$

and then

$$A_1 + B_1K_1 = \begin{pmatrix} -11 & -10 \\ 1 & -22 \end{pmatrix},$$

$$A_2 + B_2K_2 = \begin{pmatrix} -22 & 1 \\ -10 & -11 \end{pmatrix},$$

$$B_{m1} = B_{m2} = \begin{pmatrix} 21 \\ 21 \end{pmatrix}, D_{m1} = D_{m2} = \begin{pmatrix} 1 \\ 1 \end{pmatrix}.$$

The second step is to design the filters  $G_{fi}(s)$ ,  $i \in \Lambda$ . According to [27], the filters can be designed as

$$G_{f1}(s) = G_{f2}(s) = \frac{a_1s + (a_2 - \omega_0^2)}{s^2 + a_1s + a_2},$$

where  $\omega_0 = 0.5$ ,  $a_1 = 10\omega_0$  and  $a_2 = 100\omega_0^2$ .

According to the results in [3], the lower bound of ADT  $\tau_a^* = \frac{1}{2} \log(10) = 1.1513$ . According to Theorem 6, the following performance:

$$\lim_{t \rightarrow \infty} x(t) = x_m(t), \lim_{t \rightarrow \infty} x_1(t) = c(t)$$

is achieved under any switching signal with ADT  $\tau_a \geq 1.1513$ .

With the initial condition:  $x(0) = (1, -2)^T$  and the following switching path:

$$\sigma(t) = \begin{cases} 2, & t \in [t_{2k}, t_{2k+1}), t_{2k+1} - t_{2k} = 1.1513 + rand \\ 1, & t \in [t_{2k+1}, t_{2k+2}), t_{2k+2} - t_{2k+1} = 1.1513 \end{cases},$$

where  $k = 0, 1, 2, \dots$ , and  $rand \in (0, 1)$  is a random number, the simulation results are shown in Fig. 1.

From Fig. 1, it can be observed that the state  $x(t)$  of the system (24) asymptotically tracks the state  $x_m(t)$  of the reference model (25) quickly and the state  $x_1(t)$  also asymptotically tracks the command  $c(t)$  quickly. The simulation results show that the proposed control is very effective in achieving the robust tracking of a class of linear switched systems with model uncertainty and external disturbance.

## V. CONCLUSIONS

In this paper, the robust tracking problem of a class of linear switched systems with both system uncertainty and external disturbance has been investigated. Firstly, some new stability results about linear switched systems with disturbance have been presented in two cases: one is under arbitrary switching paths, the other is under switching paths restricted with average dwell time. Then, based on the obtained stability results and the existing UDE-based control method, the asymptotic stability of the linear switched system has been established in the above mentioned two cases, which guaranteed that the states of the linear switched systems can asymptotically track the command in the presence of both uncertainty and disturbance. Finally, a numerical example is provided to verify effectiveness of the proposed method.

## REFERENCES

- [1] D. Liberzon and A. S. Morse, "Basic problems in stability and design of switched systems," *IEEE Control Systems*, vol. 19, no. 5, pp. 59–70, 1999.
- [2] E. Skafidas, R. J. Evans, A. V. Savkin, and I. R. Petersen, "Stability results for switched controller systems," *Automatica*, vol. 35, no. 4, pp. 553–564, 1999.
- [3] R. Guo and Y. Wang, "Stability analysis for a class of switched linear systems," *Asian Journal of Control*, vol. 14, no. 3, pp. 817–826, 2012.
- [4] A. Bemporad, G. Ferrari-Trecate, M. Morari *et al.*, "Observability and controllability of piecewise affine and hybrid systems," *IEEE Transactions on Automatic control*, vol. 45, no. 10, pp. 1864–1876, 2000.
- [5] D. Cheng *et al.*, "Controllability of switched bilinear systems," *IEEE Transactions on Automatic Control*, vol. 50, no. 4, pp. 511–515, 2005.
- [6] R. A. DeCarlo, M. S. Branicky, S. Pettersson, and B. Lennartson, "Perspectives and results on the stability and stabilizability of hybrid systems," in *Proceedings of the IEEE*, vol. 88, no. 7, pp. 1069–1082, 2000.
- [7] D. Cheng, L. Guo, Y. Lin, Y. Wang *et al.*, "Stabilization of switched linear systems," *IEEE Transactions on Automatic control*, vol. 50, no. 5, pp. 661–666, 2005.
- [8] H. Lin and P. J. Antsaklis, "Stability and stabilizability of switched linear systems: a survey of recent results," *IEEE Transactions on Automatic Control*, vol. 54, no. 2, pp. 308–322, 2009.
- [9] K. S. Narendra and J. Balakrishnan, "A common Lyapunov function for stable LTI systems with commuting A-matrices," *IEEE Transactions on Automatic Control*, vol. 39, no. 12, pp. 2469–2471, 1994.

- [10] D. Liberzon, R. Tempo *et al.*, "Common Lyapunov functions and gradient algorithms," *IEEE Transactions on Automatic Control*, vol. 49, no. 6, pp. 990–994, 2004.
- [11] M. S. Branicky, "Multiple Lyapunov functions and other analysis tools for switched and hybrid systems," *IEEE Transactions on Automatic Control*, vol. 43, no. 4, pp. 475–482, 1998.
- [12] R. Guo, "Stability analysis of a class of switched nonlinear systems with an improved average dwell time method," in *Abstract and Applied Analysis*, vol. 2014. Hindawi Publishing Corporation, 2014.
- [13] Q. Wang, Y. Hou, and C. Dong, "Model reference robust adaptive control for a class of uncertain switched linear systems," *International Journal of Robust and Nonlinear Control*, vol. 22, no. 9, pp. 1019–1035, 2012.
- [14] L. Long and J. Zhao, "Adaptive disturbance rejection for strict-feedback switched nonlinear systems using multiple lyapunov functions," *International Journal of Robust and Nonlinear Control*, vol. 24, no. 13, pp. 1887–1902, 2014.
- [15] J. Yang, S. Li, and X. Yu, "Sliding-mode control for systems with mismatched uncertainties via a disturbance observer," *IEEE Transactions on Industrial Electronics*, vol. 60, no. 1, pp. 160–169, 2013.
- [16] Y. Liu, Y. Niu, J. Lam, and B. Zhang, "Sliding mode control for uncertain switched systems with partial actuator faults," *Asian Journal of Control*, vol. 16, no. 6, pp. 1779–1788, 2014.
- [17] D. Yang and J. Zhao, "Composite anti-disturbance control for switched systems via mixed state-dependent and time-driven switching," *IET Control Theory & Applications*, vol. 10, no. 16, pp. 1981–1990, 2016.
- [18] D. Belkhiat, N. Messai, and N. Manamanni, "Design of a robust fault detection based observer for linear switched systems with external disturbances," *Nonlinear Analysis: Hybrid Systems*, vol. 5, no. 2, pp. 206–219, 2011.
- [19] D. Wang, W. Wang, and P. Shi, "Exponential  $H_\infty$  filtering for switched linear systems with interval time-varying delay," *International Journal of Robust and Nonlinear Control*, vol. 19, no. 5, pp. 532–551, 2009.
- [20] M. Hajjahmadi, B. De Schutter, and H. Hellendoorn, "Robust  $H_\infty$  switching control techniques for switched nonlinear systems with application to urban traffic control," *International Journal of Robust and Nonlinear Control*, vol. 26, no. 6, pp. 1286–1306, 2016.
- [21] C. Li and J. Zhao, "Robust passivity-based  $H_\infty$  control for uncertain switched nonlinear systems," *International Journal of Robust and Nonlinear Control*, vol. 26, no. 14, pp. 3186–3206, 2016.
- [22] Q.-C. Zhong and D. Rees, "Control of uncertain LTI systems based on an uncertainty and disturbance estimator," *Journal of Dynamic Systems, Measurement, and Control*, vol. 126, no. 4, pp. 905–910, 2004.
- [23] K. Youcef-Toumi and O. Ito, "A time delay controller for systems with unknown dynamics," *Journal of Dynamic Systems, Measurement, and Control*, vol. 112, no. 1, pp. 133–142, 1990.
- [24] Q.-C. Zhong, A. Kuperman, and R. Stobart, "Design of UDE-based controllers from their two-degree-of-freedom nature," *International Journal of Robust and Nonlinear Control*, vol. 21, no. 17, pp. 1994–2008, 2011.
- [25] A. Kuperman and Q.-C. Zhong, "UDE-based linear robust control for a class of nonlinear systems with application to wing rock motion stabilization," *Nonlinear Dynamics*, vol. 81, no. 1-2, pp. 789–799, 2015.
- [26] B. Ren, Q.-C. Zhong, and J. Chen, "Robust control for a class of nonaffine nonlinear systems based on the uncertainty and disturbance estimator," *IEEE Transactions on Industrial Electronics*, vol. 62, no. 9, pp. 5881–5888, 2015.
- [27] B. Ren, Q. C. Zhong, and J. Dai, "Asymptotic reference tracking and disturbance rejection of UDE-based robust control," *IEEE Transactions on Industrial Electronics*, vol. 64, no. 4, pp. 3166–3176, 2017.