<u>EX 10.3.1</u>: The lifetimes of three light bulb brands were measured:

BULB BRAND	(BULB LIFETIMES in yrs)				
Brand 1 $(x_{1\bullet})$	$9.22, \ 9.07, \ 8.95, \ 8.98, \ 9.54$				
Brand 2 $(x_{2\bullet})$	8.92, 8.88, 9.10				
Brand 3 $(x_{3\bullet})$	9.08, 8.99, 9.06, 8.93				

(a) Formulate this experiment as a 1-Factor ANOVA fixed effects linear model.

		μ =	Ξ	Common population mean lifetime of the three bulb brands
$X_{ij} = \mu + \alpha_i^A + E_{ij}$	where	$\alpha^A_i \equiv$	Ξ	Lifetime deviation from μ due to Brand <i>i</i> bulb
		E_{ij} =	Ξ	Lifetime deviation from μ due to random error/noise

(b) Perform the appropriate 1-Factor ANOVA at significance level $\alpha = 0.01$ – compute both the *F*-cutoff and P-value.

$$\begin{split} I &= 3; \ J_1 = 5, \ J_2 = 3, \ J_3 = 4 \implies n = \sum_i J_i = 5 + 3 + 4 = 12 \implies \nu_{res} = n - I = 12 - 3 = 9, \ \nu_A = I - 1 = 3 - 1 = 2 \\ \hline x_{1\bullet} &:= \frac{1}{I_1} \sum_{j=1}^{J_1} x_{1j} = \frac{1}{5} (9.22 + 9.07 + 8.95 + 8.98 + 9.54) = 9.152 \\ \hline x_{2\bullet} &:= \frac{1}{I_2} \sum_{j=1}^{J_2} x_{2j} = \frac{1}{3} (8.92 + 8.88 + 9.10) \approx 8.967 \\ \hline x_{3\bullet} &:= \frac{1}{I_3} \sum_{j=1}^{J_3} x_{3j} = \frac{1}{4} (9.08 + 8.99 + 9.06 + 8.93) = 9.015 \\ \hline x_{\bullet\bullet} &:= \frac{1}{T} \sum_i \bar{x}_{i\bullet} = \frac{1}{3} (9.152 + 8.967 + 9.015) \approx 9.045 \\ s_1^2 &:= \frac{1}{J_{1-1}} \sum_{j=1}^{J_1} (x_{1j} - \bar{x}_{1\bullet})^2 = \frac{1}{5-1} \left[(9.22 - 9.152)^2 + (9.07 - 9.152)^2 + (8.95 - 9.152)^2 \\ + (8.98 - 9.152)^2 + (9.54 - 9.152)^2 \end{array} \right] = 0.05807 \\ s_2^2 &:= \frac{1}{J_{2-1}} \sum_{j=1}^{J_2} (x_{2j} - \bar{x}_{2\bullet})^2 = \frac{1}{3-1} \left[(8.92 - 8.967)^2 + (8.88 - 8.967)^2 + (9.10 - 8.967)^2 \right] = 0.01373 \\ s_3^2 &:= \frac{1}{J_{3-1}} \sum_{j=1}^{J_3} (x_{3j} - \bar{x}_{3\bullet})^2 = \frac{1}{4-1} \left[(9.08 - 9.015)^2 + (8.99 - 9.015)^2 + (9.06 - 9.015)^2 \\ + (8.93 - 9.015)^2 \right] \approx 0.0047 \\ SS_{res} &:= \sum_i (J_i - 1)s_i^2 = (5-1)(0.05807) + (3-1)(0.01373) + (4-1)(0.0047) = 0.27384 \\ SS_A &:= \sum_i J_i (X_{i\bullet} - \bar{x}_{\bullet\bullet})^2 = 5(9.152 - 9.045)^2 + 3(8.967 - 9.045)^2 + 4(9.015 - 9.045)^2 = 0.0791 \\ MS_{res} &:= \frac{SS_{res}}{\nu_{res}} = \frac{0.27384}{9} = 0.0304, \ MS_A &:= \frac{SS_A}{\nu_A} = \frac{0.0791}{2} = 0.03955 \\ f_A &:= \frac{MS_A}{MS_{res}} = \frac{0.03955}{0.0304} \approx 1.301 \\ \end{split}$$

By hand: $f_{\nu_A,\nu_{res};\alpha}^* = f_{2,9;0,01}^* \stackrel{LOOKUP}{\approx} 8.02$ By SW: $p_A := \mathbb{P}(F > f_A) = 1 - \Phi_F(f_A;\nu_A,\nu_{res}) = 1 - \Phi_F(1.301;\nu_1 = 2,\nu_2 = 9) \stackrel{SW}{\approx} 1 - 0.6811 \approx 0.3189$

Since either by hand, $f_A \approx 1.301 < 8.02 \approx f_{\nu_A,\nu_{res};\alpha}^*$, or, by software, $p_A \approx 0.3189 > 0.01 = \alpha$, accept H_0^A . There's not enough evidence from the experiment to claim that at least two of the bulb brands' avg. lifetimes differ. (c) Summarize everything in an 1-Factor ANOVA table.

1-Factor ANOVA Table (Significance Level $\alpha = 0.01$)									
Variatio Source	n df	Sum of Squares	Mean Square	F Stat Value	P-value	Decision			
Factor A	. 2	0.07910	0.03955	1.301	0.3189	Accept H_0^A			
Unknown	n 9	0.27384	0.0304						
Total	11	0.35294							

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EX 10.3.2: Dentists use resin composites and ceramic fillings among others for cavities in teeth. The shear bond strengths of resin composite-ceramic bonds formed from three possible configurations (conventional, all-composite, reversed) were measured (in MPa) and summarized in the following table:

GROUP:	SAMPLE SIZE:	MEAN:	STD DEV:
Conventional	9	$\overline{x}_{1\bullet} = 10.37$	$s_1 = 1.99$
All-Composite	8	$\overline{x}_{2\bullet} = 21.82$	$s_2 = 2.45$
Reversed	6	$\overline{x}_{3\bullet} = 18.02$	$s_3 = 2.52$

This table and all the details regarding the experiment can be found in the following paper:

A. Della Bona, R. van Noort, "Shear vs. Tensile Bond Strength of Resin Composite Bonded to Ceramic", *Journal of Dental Research*, **74** (1995), 1591-1596.

(a) Formulate this experiment as a 1-Factor ANOVA fixed effects linear model.

 $\mu \equiv \text{Common population mean shear bond strength of the three configurations}$ $X_{ij} = \mu + \alpha_i^A + E_{ij} \text{ where } \alpha_i^A \equiv \text{Shear bond strength deviation from } \mu \text{ due to } i^{th} \text{ configuration}$ $E_{ij} \equiv \text{Shear bond strength deviation from } \mu \text{ due to random error/noise}$

(b) Perform the appropriate 1-Factor ANOVA at significance level $\alpha = 0.05$ – compute both the F-cutoff and P-value.

 $I = 3; \ J_1 = 9, \ J_2 = 6, \ J_3 = 8 \implies n = \sum_i J_i = 9 + 6 + 8 = 23 \implies \nu_{res} = n - I = 23 - 3 = 20, \ \nu_A = I - 1 = 3 - 1 = 2$

 $\overline{x}_{\bullet\bullet} := \frac{1}{I} \sum_{i} \overline{x}_{i\bullet} = \frac{1}{3} (10.37 + 21.82 + 18.02)$ $SS_{res} := \sum_{i} (J_{i} - 1)s_{i}^{2} = (9 - 1) \cdot 1.99^{2} + (8 - 1) \cdot 2.45^{2} + (6 - 1) \cdot 2.52^{2} = 105.4503$ $SS_{A} := \sum_{i} J_{i} (\overline{x}_{i\bullet} - \overline{x}_{\bullet\bullet})^{2} = 9 \cdot (10.37 - 16.737)^{2} + 8 \cdot (21.82 - 16.737)^{2} + 6 \cdot (18.02 - 16.737)^{2} = 581.4198$

$$MS_{res} := \frac{SS_{res}}{\nu_{res}} = \frac{105.4503}{20} = 5.272515, MS_A := \frac{SS_A}{\nu_A} = \frac{581.4198}{2} = 290.7099$$
$$f_A := \frac{MS_A}{MS_{res}} = \frac{290.7099}{5.272515} \approx 55.1369$$

By hand: $f_{\nu_A,\nu_{res};\alpha}^* = f_{2,20;0.05}^* \overset{LOOKUP}{\approx} \mathbf{3.49}$ By SW: $p_A := \mathbb{P}(F > f_A) = 1 - \Phi_F(f_A;\nu_A,\nu_{res}) = 1 - \Phi_F(55.1369;\nu_1 = 2,\nu_2 = 20) \overset{SW}{\approx} 1 - 0.999999992727 \approx \mathbf{7.273} \times \mathbf{10}^{-9}$

Since either by hand, $f_A \approx 55.1369 \gg 3.49 \approx f^*_{\nu_A,\nu_{res};\alpha}$, or, by software, $p_A \approx 7.273 \times 10^{-9} \ll 0.05 = \alpha$, reject H_0^A . There's enough evidence from the experiment to claim that at least two of the bond configs' avg. shear bond strengths differ.

(c) Perform the appropriate Tukey-Kramer Complete Pairwise Post-Hoc Comparison.

$$\begin{split} w_{(12)} &= q_{I,\nu_{res};\alpha}^* \cdot \sqrt{\mathrm{MS}_{res} \cdot \frac{1}{2} \left(\frac{1}{J_1} + \frac{1}{J_3} \right)} \approx q_{3,20;0.05}^* \cdot \sqrt{5.272515 \cdot \frac{1}{2} \left(\frac{1}{9} + \frac{1}{8} \right)} & \overset{LOOKUP}{\approx} 3.58 \cdot \sqrt{5.272515 \cdot \frac{17}{144}} \approx 2.824 \\ w_{(13)} &= q_{I,\nu_{res};\alpha}^* \cdot \sqrt{\mathrm{MS}_{res} \cdot \frac{1}{2} \left(\frac{1}{J_1} + \frac{1}{J_2} \right)} \approx q_{3,20;0.05}^* \cdot \sqrt{5.272515 \cdot \frac{1}{2} \left(\frac{1}{9} + \frac{1}{6} \right)} & \overset{LOOKUP}{\approx} 3.58 \cdot \sqrt{5.272515 \cdot \frac{5}{36}} \approx 3.064 \\ w_{(23)} &= q_{I,\nu_{res};\alpha}^* \cdot \sqrt{\mathrm{MS}_{res} \cdot \frac{1}{2} \left(\frac{1}{J_2} + \frac{1}{J_3} \right)} \approx q_{3,20;0.05}^* \cdot \sqrt{5.272515 \cdot \frac{1}{2} \left(\frac{1}{9} + \frac{1}{6} \right)} & \overset{LOOKUP}{\approx} 3.58 \cdot \sqrt{5.272515 \cdot \frac{5}{36}} \approx 3.064 \\ w_{(23)} &= q_{I,\nu_{res};\alpha}^* \cdot \sqrt{\mathrm{MS}_{res} \cdot \frac{1}{2} \left(\frac{1}{J_2} + \frac{1}{J_3} \right)} \approx q_{3,20;0.05}^* \cdot \sqrt{5.272515 \cdot \frac{1}{2} \left(\frac{1}{8} + \frac{1}{6} \right)} & \overset{LOOKUP}{\approx} 3.58 \cdot \sqrt{5.272515 \cdot \frac{5}{36}} \approx 3.139 \\ \overline{x}_{(2)\bullet} \notin \left(\overline{x}_{(1)\bullet}, \overline{x}_{(1)\bullet} + w_{(12)} \right), \quad \overline{x}_{(3)\bullet} \notin \left(\overline{x}_{(1)\bullet}, \overline{x}_{(1)\bullet} + w_{(13)} \right), \quad \overline{x}_{(3)\bullet} \in \left(\overline{x}_{(2)\bullet}, \overline{x}_{(2)\bullet} + w_{(23)} \right) \\ \overline{x}_{(1)\bullet} \quad \overline{x}_{(2)\bullet} \quad \overline{x}_{(3)\bullet} \\ \overline{x}_{1\bullet} \quad \overline{x}_{3\bullet} \quad \overline{x}_{2\bullet} \end{split}$$

 $10.37 \ \underline{18.02} \ \underline{21.82}$

The experiment suggests that the all-composite and reversed configurations each have a significantly higher shear bond strength than the conventional.

The experiment suggests that there is not a significant difference in shear bond strength between the all-composite and reversed configurations.

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